

Design and Development of Adaptive Headlight System (AHS)

Manish Bhargao, Student, MIT College of Engineering, Pune, India, mbhargao1997@gmail.com

Mihir Sonawane, Student, MIT College of Engineering, Pune, India, mihirsss10@gmail.com

Prof Abhijit.A.Kadam, Professor, MIT College of Engineering, Pune, India, aakadam31@gmail.com

Gopal Patil, Student, MIT College of Engineering, Pune, India, patilgopal500@gmail.com

Rahul Yadav, Student, MIT College of Engineering, Pune, India, rahul225599@gmail.com

Abstract In today's fast moving vehicle scenario, road safety is of utmost importance. Many people have lost their lives while travelling, due to a road accident. So we should mitigate such accidents if we wish to travel safely. To cater this cause, we propose an adaptive steering controlled headlight setup. The system can be adopted in any type of four wheel vehicles/trucks or trailers etc. Without being an economic burden on the end user. The notion of steering controlled headlight is not new, but its adaptability according to the steering turning angle is its novel part. A lot of companies have developed technologies that incorporate turn able headlight to better illuminate the path, but these technologies are quite expensive and continue to be distant from the majority of car owners. So we felt the need of developing a mechanism that incorporates few simple components like gears, linkages etc. And can be readily fitted onto any steering column without much of a design variations. The setup contains a gear mounted on the steering column and it is mesh with the semicircular gear which is mounted on an axis parallel to the steering column. A linkage or wire mechanism is used to transmit the rotating motion to the headlight. The headlight is designed so that it has 1 degree of freedom i.e. it can rotate about its axis. This setup will be of huge aid to the driver, as it will permit him to see the incoming obstructions in hilly areas or in the regions with sharp turns as it provides a better illuminated path by the virtue of adaptable headlights.

Keywords —Adaptive Headlight System (AHS), Bevel Gears, Spur Gears, Safety, Gear Ratio

I. INTRODUCTION

Safety is the biggest concern for automobile manufacturers and also for the driver of that automobile. The manufacturers who installs latest safety equipment in their vehicle wins the trust of its customers and hence makes it big in the market. Adaptive headlight is one such attempt. In fact, adaptive headlight technology first appeared on a 1960s Citroën DS. The French automaker developed a quad-headlight system where the inner pair of lights swiveled with the front wheels, making it the first car to "see" around corners.

Nowadays big companies such as Ford have patented their own adaptive headlight system. Based on stepper motors and sensors for safety purposes. But these systems are very costly. These system are precise and safety on road is guarantee.

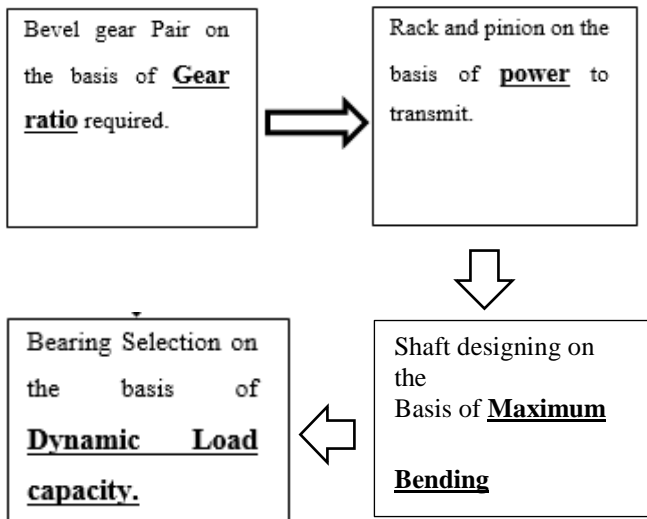
II. DESIGN METHODOLOGY

Two Spur gears will be installed on the of **rack and pinion** mechanism of the steering of the car.

This gears will rotate along with the pinion of the Rack and pinion. By connecting a shaft to the spur gears a **bevel gears** assembly can be constructed having a suitable **gear ratio**.

This gear ratio will determine the actual relation between the angle of rotation of steering wheel and the angle of rotation of the headlight.

The headlight can be mounted of the Bevel gear which will be connected to the shaft



Design Flowchart

DESIGN OF BEVEL GEAR

For the design of bevel gears, certain assumption have to be made.

Initial Known data:

The material selected is C.I FG 220 ($S_{ut}=220\text{Mpa}$)

Pressure angle (ϕ) = 20°

Module of gears= 3

Gear ratio = 3:1

F.O. $S_{bending}=2$

We know that,

Minimum number of teeth on Bevel pinion is given by:

$$Z_{min} = \frac{2h_a \cos \gamma_p}{m \sin^2 \phi} \dots\dots\dots(\text{eq 2.1})$$

2.1)

Putting $h_a=1m$,

$$\gamma_p = \tan^{-1} \frac{1}{G}$$

$$\gamma_p = \tan^{-1} \frac{1}{3}$$

$\Phi=20^\circ$

Substituting the values in eq 3.1.1

We have, Number of teeth on Bevel Pinion (Z_p) = 18

We know that,

$$m = \frac{d}{z}$$

Hence, $d_p=54$

$G=3$ hence $Z_g=54$

$d_g=162\text{mm}$

Now, Pitch Cone diameter

$$AO = \sqrt{(d_p/2)^2 + (d_g/2)^2}$$

$$AO = \sqrt{(54/2)^2 + (162/2)^2}$$

$AO=85.38\text{mm}$

Face width b,

$$b = \frac{AO}{3} \text{ or } 10m \text{ } \} \text{ whichever is smaller}$$

$b=28.71$ or 30mm

Selecting $b=28.71\text{mm}$

Consider Bending Failure

Bending force acting is given by,

$$F_b = \sigma_{bp} b m Y'_{fp} \left(1 - \frac{b}{AO}\right) \dots\dots\dots \text{Eq(2.2)}$$

$$\sigma_{bp} = \frac{S_{ut}}{3} = \frac{220}{3} = 73.33 \text{MPa}$$

$b = 28.4\text{mm}$

$m=3$

$$Y'_{fp} = 0.484 - \frac{2.87}{Z'_{fp}}$$

Here,

Z'_{fp} is formative number of teeth.

$$Z'_{fp} = \frac{Z_p}{\cos \gamma_p} = \frac{18}{0.9487} = 18.97$$

Similarly,

$$Z'_g = 170.71$$

Substituting the obtained values in eq 3.1.2

$$\text{We have, } (F_b = 73.33 * 28.44 * 3 * 0.3327 * \left(1 - \frac{28.4}{85.38}\right))$$

$$F_b = 1385.7 \text{ N}$$

Consider Wear Failure

Wear failure of gear is given by the following expression

$$F_w = \frac{0.75 d_p b Q' K}{\cos \gamma_p} \dots\dots\dots(\text{Eq 2.3})$$

2.3)

Load stress factor

$$K = 0.21 \left(\frac{BHN}{100}\right)^2$$

$$K = 0.21 \left(\frac{250}{100}\right)^2$$

$K=1.31$

Ratio Factor for gear pair

$$Q' = \frac{2Z'_g}{Z'_g + Z'_p}$$

$$Q' = \frac{2170.71}{170.71 + 18.97}$$

$Q' = 1.8$

$$F_w = \frac{0.75 * 54 * 28.4 * 1.8 * 1.31}{0.9488}$$

$F_w = 2858.79 \text{ N}$

Comparing F_b and F_w we observe that $F_b < F_w$

Hence, Designing Gear for Failure

$$F_{eff} = \frac{F_t}{K_v} \dots \dots \dots \text{(Eq 2.4)}$$

Here , K_v is called as the Barth Factor or velocity Factor.

$$K_v = \frac{5.6}{5.6 + \sqrt{V}}$$

V is Pitch line velocity and is given by;

$$V = \frac{\pi d_p n_p}{60000}$$

$$V = 0.8482 \text{ m/s}$$

Putting this value is expression of K_v we have

$$K_v = 0.8587$$

Putting the value in eq 3.1.4 we have

$$F_{eff} = \frac{F_t}{0.8567}$$

$$F_b = F.O.S * F_{eff} \dots \dots \dots \text{(Eq 2.5)}$$

$$1038.96 = 2 * \frac{F_t}{0.8567}$$

$$F_t = 593.56 \text{ N}$$

Power that is transmitted is calculated as

$$P = F_t * v$$

$$P = 503 \text{ Watts}$$

Forces on Bevel gear are given as

$$\begin{aligned} F_{rp} &= F_{aG} = F_t \tan \phi \cos \gamma_p \\ &= 593.56 * \tan 20 * \cos 18.43 \\ &= 157.69 \text{ N} \end{aligned}$$

$$\begin{aligned} F_{ap} &= F_{ap} = F_t \tan \phi \cos \gamma_g \\ &= 593.56 * \tan 20 * \cos 71.56 \\ &= 68.33 \text{ N} \end{aligned}$$

Bevel gear Results

Z_p	18	F_t	593.56 N
Z_g	54	$F_{rp} = F_{ag}$	204.95 N
m	3	$F_{ap} = F_{rg}$	68.33
d_p	54mm		
d_g	162mm		

Table 1 Bevel gear results

SPUR GEAR CALCULATIONS

For the design of Rack and Pinion some data is to assumed

Initial Data

Material for Rack C.I FG 220 ($S_{ut} = 220 \text{ Mpa}$)

Lewis Form Factor $Y_p = 0.3644$

Lewis form factor $Y_r = 0.484$

F.O.S = 1.5

Pressure angle (ϕ) = 20°

Machining Factor (K_a) = 1

Application Factor (K_m) = 1.05

Barth Velocity factor (K_v) = 0.9836

Tangential Force is transmitted by the rack to the spur pinion

Hence, Tangential Force is given as

$$F_t = \frac{2T_m}{Z_p m} \dots \dots \dots \text{(Eq 3.1)}$$

Here T_m is the torque which is given by,

$$T_m = \frac{P60000}{2\pi n_p}$$

$$T_m = \frac{503 * 60000}{2\pi * 300}$$

$$T_m = 16010.9 \text{ KN}$$

Substituting the value of T_m in Eq 3.2.1

$$F_t = \frac{1334.2}{m} \dots \dots \dots \text{(Eq 3.2)}$$

3.2)

Now Applying Lewis Equation for Bending

$$F_b = \sigma_{bp} b m Y_p$$

$$F_b = \frac{S_{ut}}{3} 10m m 0.3644$$

$$F_b = 267.21 m^2 \dots \dots \dots \text{Eq(3.3)}$$

Now we know F.O.S

$$F_b = F.O.S * F_{eff}$$

$$F_b = F.O.S * \frac{K_a K_m F_t}{K_v}$$

$$F_b = 1.5 * \frac{1.05 * 1}{0.9836} F_t \dots \dots \dots \text{(eq 3.4)}$$

$$F_b = 1.601 F_t \dots \dots \dots \text{(eq 3.5)}$$

Putting equation 3.3 and 3.4 in

$$267.21 m^2 = 1.601 * \frac{1334.2}{m}$$

$$\Rightarrow m^3 = \frac{1.601 * 1334.2}{267.21} = 2.86$$

$$m = 1.99 \approx 2$$

Now pitch line velocity is given by;

$$V = \frac{\pi d_p n_p}{60000}$$

$$V = \frac{\pi 48 * 300}{60000}$$

$$V = 0.75 \text{ m/s}$$

Tangential Force is given as

$$F_t = \frac{P}{V} = \frac{T_p}{\frac{d_p}{2}}$$

$$F_t = \frac{16010.9}{24} = 667.12 \text{ N}$$

Now calculating the forces associated with the Gear

$$F_r = F_t * \tan \phi$$

$$F_r = 667.12 * \tan 20$$

$$F_r = 242.81 \text{ N}$$

Spur Gear Results

Material of Rack and pinion	C.I FG 220 (Sut=220 Mpa)
Number of teeth on pinion	$Z_p = 24$
Module	2
Tangential force (Ft)	667.12 N
Radial Force (Fr)	242.81 N

Table 2 Spur gear results

III. SHAFT CALCULATION PROCEDURE

- Step 1: Calculate the torque on the shaft from power
- Step 2: Find the torsional stress in the shaft
- Step 3: Calculate the loads coming from gears, belts
- Step 4: Calculate the bending moment due to the acting forces. If necessary combine the forces acting
- Step 5: Calculate the bending stress in the shaft
- Step 6: Combine the bending stress and the torsional stress using the theories of stress should not be selected.

IV. ANALYSIS

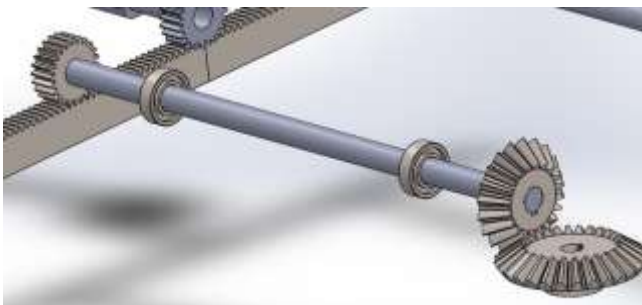


Fig1 Shaft CAD

Consider the shaft
The SFD and BMD in the horizontal and Vertical Plane are as follows

- In Horizontal Plane

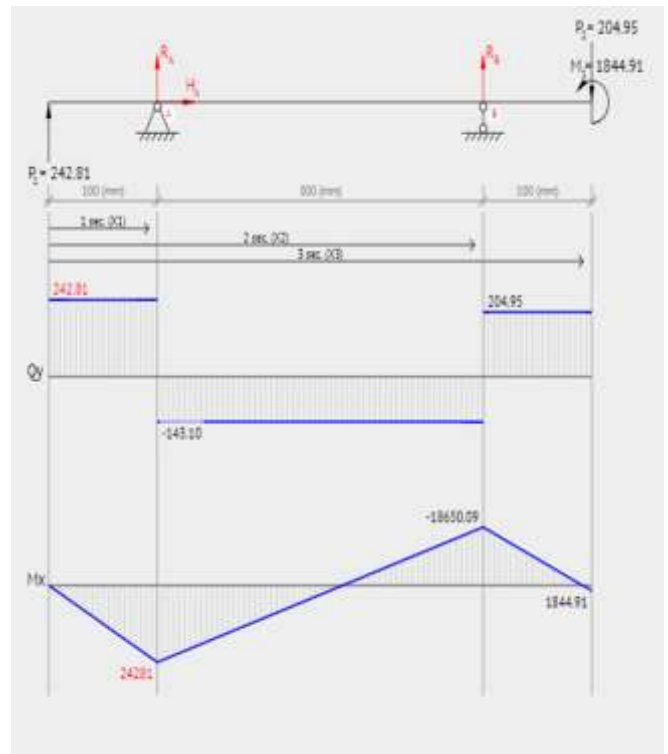


Fig 2 SFD BMD horizontal plane

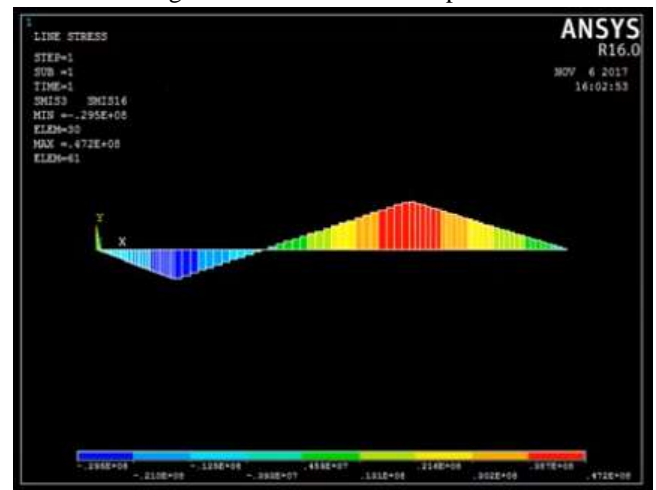


Fig 3 BMD on ANSYS APDL

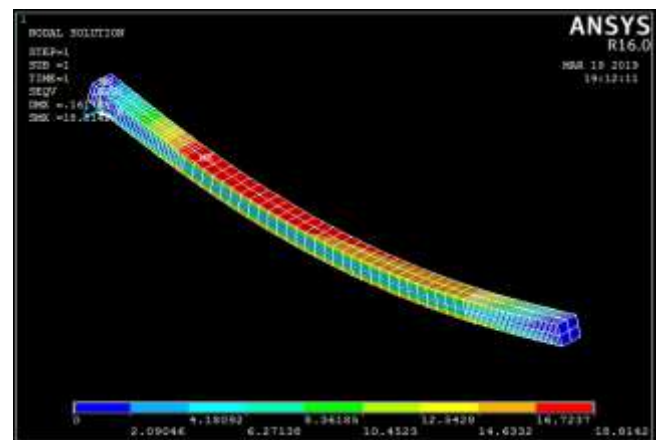


Fig 4 Deflection of shaft

- In Vertical Plane

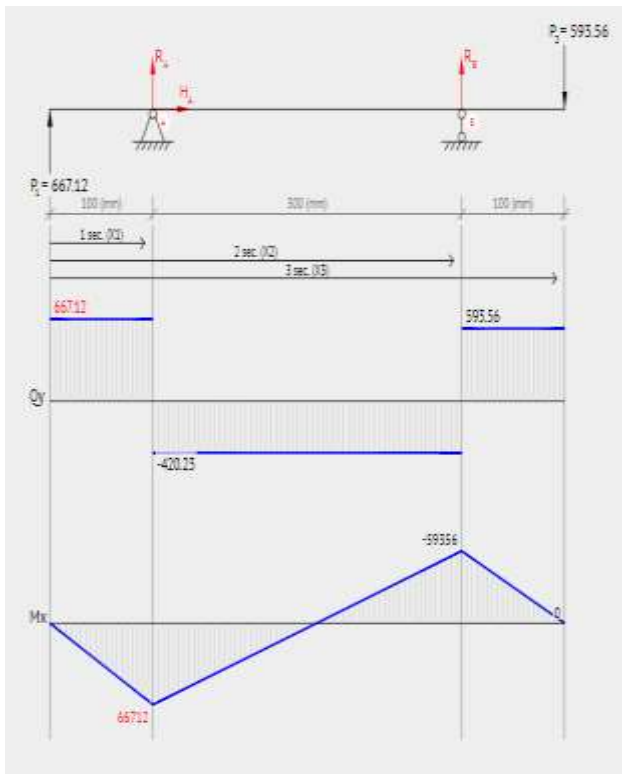


Fig 5 SFD BMD of Vertical shaft

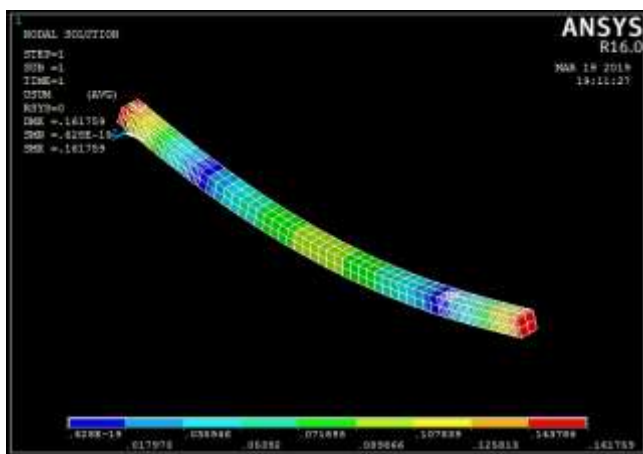


Fig 6 Von Mises stresses

V. CONCLUSION

After following the designing procedure for Rack and pinion, bevel gear pair, Shaft and bearing the final assembly is done in CAD software Solid works.

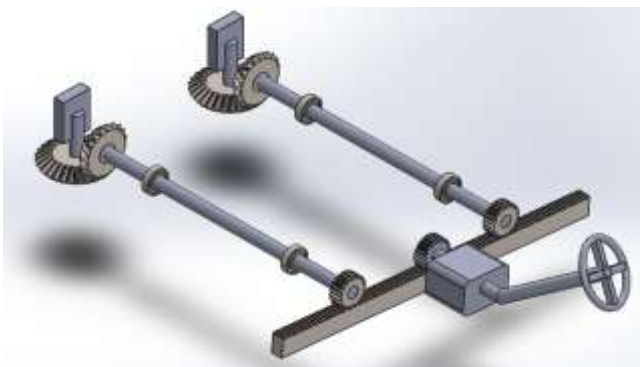


Fig 7 Final CAD assembly

VI. ADVANTAGES

- Enhanced existing functionality.
- Improved visibility.
- Simple Design.
- Decreased number of night time accidents.
- Increased safety for drivers and pedestrians.

VII. DISADVANTAGES

- Less precision than electronic system.
- Increased steering effort.
- Increased weight.
-

ACKNOWLEDGMENT

I am very much obliged to Project guide, Prof. A. A. Kadam in Mechanical Engineering Department, for helping and giving proper guidance. His timely suggestions made it possible to complete this seminar for me. I will fail in my duty if I won't acknowledge a great sense of gratitude to the Director - Prof. R. V. Pujeri, Principal - Prof. (Dr.) A. S. Hiwale, Head of Mechanical Dept. - Prof (Dr.) S. B. Barve and the entire staff of members of Mechanical Engineering Dept. for their cooperation.

REFERENCES

- [1] Alexander, G. J. and Lunenfeld, H. (1990), "A users' guide to positive guidance, third ed.," Report No. FHWA-SA-90-017, U.S. Department of Transportation, Federal Highway Administration, Washington, DC pp. 1-39
- [2] D. Neunzig and R. Lachmayer, "Lighting and Driver Assistances Systems for Improving Vehicle Safety," ATZ Worldwide 6/2002, Vol. 104, pp 13-17. Jul. 1993.
- [3] Japanese Patent Application Laid-Open No. H8-192674R..
- [4] US Patent No. 6,309,082, Inventor - Tien-Ching Wu.
- [5] F10 M5carblog.blogspot.in/2013/02/steering
- [6] V. B. Bhandari (1994), Design of machine elements, third edition Page 334,573
- [7] Thomas D Gillespie, Fundamentals of vehicle dynamics page no 289-291
- [8] J. G. Kreifeldt, "An analysis of surface-detected EMG as an amplitude-modulated noise," presented at the 1989 Int. Conf. Medicine and Biological Engineering, Chicago, IL.
- [9] J. Williams, "Narrow-band analyzer (Thesis or Dissertation style)," Ph.D. dissertation, Dept. Elect. Eng., Harvard Univ., Cambridge, MA, 1993.