

# Response of a parallel $\mathcal{L}$ - $\mathcal{C}$ - $\mathcal{R}$ network connected to an excitation source providing a constant current by matrix method

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**Abstract:** In most of the branches of the engineering, the analysis of electric networks containing elements like inductor  $\mathcal{L}$ , capacitor  $\mathcal{C}$ , and resistor  $\mathcal{R}$  is an essential course. The response of such networks is generally obtained by adopting the classical method or Laplace transform. In this paper, we discuss a matrix method for obtaining the response of a parallel electric network of an inductor, a capacitor, and a resistor, connected to an excitation source providing a constant current. The response obtained will be in the form an equation for the voltage across the parallel  $\mathcal{L}$ -  $\mathcal{C}$ -  $\mathcal{R}$  network connected to an excitation source providing a constant current. The nature of this response (i.e. voltage) depends on the values of elements  $\mathcal{L}$ ,  $\mathcal{C}$ , and  $\mathcal{R}$  of the network.

**Keywords:** Constant current, Excitation source, Electric network, Response, Voltage.

## I. INTRODUCTION

An electric circuit of parallel  $\mathcal{L}$ -  $\mathcal{C}$ -  $\mathcal{R}$  network comprises of three basic elements namely an inductor having inductance  $\mathcal{L}$ , a capacitor having capacitance  $\mathcal{C}$ , and a resistor having resistance  $\mathcal{R}$ , connected to a to an excitation source providing a constant current. The electric elements like an inductor, a capacitor and a resistor are passive elements since these elements don't have the ability to transfer non – zero average power in an infinite time interval whereas, the elements like a current source and a voltage source are active elements since these elements have the ability to transfer non- zero average power in an infinite time interval. The electric circuit of parallel  $\mathcal{L}$ -  $\mathcal{C}$ -  $\mathcal{R}$  network is widely used as a tuning circuit (i.e. a filtering circuit) in the analogue radios, and have many applications in oscillatory circuits[1, 2, 3].

## II. EIGENVALUES AND EIGENVECTORS

Let  $e_{ij}$  be the elements of a matrix  $E$  of order  $n$ , then we can write the characteristic equation of  $E$  such that  $|E - \Omega I|T = 0$ , where  $T$  is a column matrix and  $\Omega$  is a constant.

This characteristic equation of  $E$  on simplifying will provide  $n$  homogeneous linear equations which have a non – trivial solution if the determinant of the coefficients of the equations is zero i.e. If

$$\begin{vmatrix} (e_{11} - \Omega) & e_{12} & e_{13} & \dots & \dots & \dots & e_{1n} \\ e_{21} & (e_{22} - \Omega) & e_{23} & \dots & \dots & \dots & e_{2n} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ e_{n1} & e_{n2} & e_{n3} & \dots & \dots & \dots & (e_{nn} - \Omega) \end{vmatrix} = 0$$
, then on expanding the determinant on left hand side of this equation,

we obtain  $n^{\text{th}}$  degree equation in  $\Omega$ , which is the characteristic equation of the matrix  $E$  and its roots are known as Eigenvalues. Corresponding to each Eigenvalue there is a column matrix  $T = [t_1 \ t_2 \ \dots \ t_n]^T$  known as Eigenvector [4, 5].

## III. FORMULATION

**To find the governing differential equation:**

Considering a parallel  $\mathcal{L}$  -  $\mathcal{C}$ -  $\mathcal{R}$  network and connect a steady current source to it through a switch  $K$  as shown in figure 1.

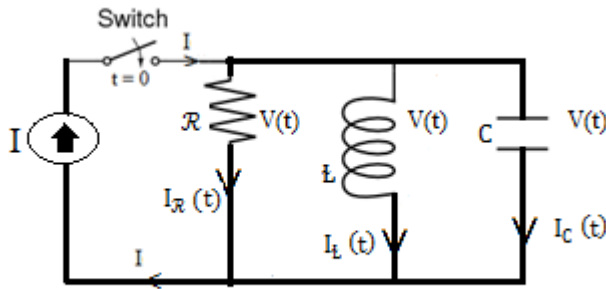


Figure 1: Parallel  $L$  -  $C$  -  $R$  network connected to a steady current source.

Let the switch is closed at the instant  $t = 0$ , then the currents flowing in the elements  $L$ ,  $C$  and  $R$  of the network are given by  $I_R(t) = \frac{V(t)}{R}$ ,  $I_L(t) = \frac{1}{L} \int V(t) dt$  and  $I_C(t) = C \mathcal{D}_t[V(t)]$ , where  $V(t)$  is the electric potential across the network elements at any instant  $t$  [1, 3].

The application of Kirchoff's current law as the switch is closed at the instant  $t = 0$  gives

$$I_R(t) + I_L(t) + I_C(t) = I$$

$$\text{Or } \frac{V(t)}{R} + \frac{1}{L} \int V(t) dt + C \mathcal{D}_t[V(t)] = I \dots (1)$$

$$\mathcal{D}_t \equiv \frac{d}{dt}$$

When we differentiate equation (1), we get a linear homogeneous differential equation of order 2 as given below:

$$\frac{1}{R} \mathcal{D}_t[V(t)] + \frac{1}{L} V(t) + C \mathcal{D}_t^2[V(t)] = 0$$

$$\text{Or } \mathcal{D}_t^2[V(t)] + \frac{1}{CR} \mathcal{D}_t[V(t)] + \frac{1}{LC} V(t) = 0 \dots (2)$$

**To obtain the solution (response):**

To find the solution of equation (2), we first write the necessary boundary conditions as follows:

- (i) Since the potential across the plates of the capacitor and the current through the inductor cannot varies instantaneously [2, 6], therefore, at the instant  $t = 0$ , then  $V(0) = 0$ .
- (ii) Since at  $t = 0$ ,  $V(0) = 0$ , therefore, equation (1) gives  $\mathcal{D}_t[V(0)] = \frac{I}{C}$ .

$$\text{On putting } V(t) = V_1(t) \dots (3)$$

$$\text{And } \mathcal{D}_t[V_1(t)] = V_2(t) \dots (4)$$

We can rewrite equation (2) as

$$\mathcal{D}_t[V_2(t)] + \frac{1}{CR} V_2(t) + \frac{1}{LC} V_1(t) = 0$$

$$\text{Or } \mathcal{D}_t[V_2(t)] = -\frac{1}{LC} V_1(t) - \frac{1}{CR} V_2(t) \dots (5)$$

We can write the differential equations (4) and (5) in a matrix form as

$$\mathcal{D}_t \begin{bmatrix} V_1(t) \\ V_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{1}{LC} & -\frac{1}{CR} \end{bmatrix} \begin{bmatrix} V_1(t) \\ V_2(t) \end{bmatrix}$$

On equating the determinant of  $\begin{bmatrix} 0 & 1 \\ -\frac{1}{LC} & -\frac{1}{CR} \end{bmatrix}$  to zero, we obtain its characteristic equation as

$$\begin{vmatrix} 0 - \Omega & 1 \\ -\frac{1}{LC} & -\frac{1}{CR} - \Omega \end{vmatrix} = 0$$

On expanding the determinant, we get

$$\Omega^2 + \frac{1}{CR} \Omega + \frac{1}{LC} = 0 \dots (6)$$

This equation (6) is quadratic in  $\Omega$  and its roots are given by

$$\Omega = \frac{-\frac{1}{CR} \pm \sqrt{\left(\frac{1}{CR}\right)^2 - \frac{4}{LC}}}{2}$$

$$\text{Or } \Omega = -\frac{1}{2CR} \pm \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}}$$

$$\text{Therefore, the roots of the equation (6) are } \Omega_1 = -\frac{1}{2CR} + \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}} \dots (7)$$

$$\text{And } \Omega_2 = -\frac{1}{2CR} - \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}} \dots (8)$$

Multiplying equations (7) and (8), we get

$$\Omega_1 \Omega_2 = \left( -\frac{1}{2CR} + \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}} \right) \left( -\frac{1}{2CR} - \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}} \right)$$

On simplifying the right hand side of this equation, we get

$$\Omega_1 \Omega_2 = \frac{1}{LC} \dots\dots\dots (9)$$

**To find Eigenvectors:**

The Eigenvector corresponding to the root  $\Omega = \Omega_1 = -\frac{1}{2CR} + \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  is given by

$$\begin{bmatrix} 0 - \Omega_1 & 1 \\ -\frac{1}{LC} & -\frac{1}{CR} - \Omega_1 \end{bmatrix} \begin{bmatrix} t_1 \\ t_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

This results

$$-\Omega_1 t_1 + t_2 = 0 \dots\dots\dots (10)$$

And

$$-\frac{1}{LC} t_1 - \left( \frac{1}{CR} + \Omega_1 \right) t_2 = 0 \dots\dots\dots (11)$$

Solving equations (10) and (11), we can write

$$\begin{bmatrix} t_1 \\ t_2 \end{bmatrix} = \begin{bmatrix} \Omega_1 + \frac{1}{CR} + 1 \\ \Omega_1 - \frac{1}{LC} \end{bmatrix}$$

And the Eigenvector corresponding to the root  $\Omega = \Omega_2 = -\frac{1}{2CR} - \frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  is given by

$$\begin{bmatrix} 0 - \Omega_2 & 1 \\ -\frac{1}{LC} & -\frac{1}{CR} - \Omega_2 \end{bmatrix} \begin{bmatrix} t_1 \\ t_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

This results

$$-\Omega_2 t_1 + t_2 = 0 \dots\dots\dots (12)$$

And

$$-\frac{1}{LC} t_1 - \left( \frac{1}{CR} + \Omega_2 \right) t_2 = 0 \dots\dots\dots (13)$$

Solving equations (12) and (13), we can write

$$\begin{bmatrix} t_1 \\ t_2 \end{bmatrix} = \begin{bmatrix} \Omega_2 + \frac{1}{CR} + 1 \\ \Omega_2 - \frac{1}{LC} \end{bmatrix}$$

The matrix of Eigenvectors is  $\begin{bmatrix} \Omega_1 + \frac{1}{CR} + 1 & \Omega_2 + \frac{1}{CR} + 1 \\ \Omega_1 - \frac{1}{LC} & \Omega_2 - \frac{1}{LC} \end{bmatrix}$ .

Let  $A = \begin{bmatrix} \Omega_1 + \frac{1}{CR} + 1 & \Omega_2 + \frac{1}{CR} + 1 \\ \Omega_1 - \frac{1}{LC} & \Omega_2 - \frac{1}{LC} \end{bmatrix}$ , then the determinant of A i.e. |A| can be written as

$$|A| = \begin{vmatrix} \Omega_1 + \frac{1}{CR} + 1 & \Omega_2 + \frac{1}{CR} + 1 \\ \Omega_1 - \frac{1}{LC} & \Omega_2 - \frac{1}{LC} \end{vmatrix}$$

On expanding the determinant and using equation (9), we obtain

$$|A| = (\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)$$

The inverse of A can be written as

$$A^{-1} = \frac{1}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \begin{bmatrix} \Omega_2 - \frac{1}{LC} & -(\Omega_2 + \frac{1}{CR} + 1) \\ -(\Omega_1 - \frac{1}{LC}) & \Omega_1 + \frac{1}{CR} + 1 \end{bmatrix}$$

**To find  $A \exp(\Omega t) A^{-1}$ :**

$A \exp(\Omega t) A^{-1} =$

$$\begin{bmatrix} \Omega_1 + \frac{1}{CR} + 1 & \Omega_2 + \frac{1}{CR} + 1 \\ \Omega_1 - \frac{1}{LC} & \Omega_2 - \frac{1}{LC} \end{bmatrix} \begin{bmatrix} \exp(\Omega_1 t) & 0 \\ 0 & \exp(\Omega_2 t) \end{bmatrix} \frac{1}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \begin{bmatrix} \Omega_2 - \frac{1}{LC} & -(\Omega_2 + \frac{1}{CR} + 1) \\ -(\Omega_1 - \frac{1}{LC}) & \Omega_1 + \frac{1}{CR} + 1 \end{bmatrix}$$

$$= \frac{1}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \times \begin{bmatrix} (\Omega_1 + \frac{1}{CR} + 1) \exp(\Omega_1 t) & (\Omega_2 + \frac{1}{CR} + 1) \exp(\Omega_2 t) \\ (\Omega_1 - \frac{1}{LC}) \exp(\Omega_1 t) & (\Omega_2 - \frac{1}{LC}) \exp(\Omega_2 t) \end{bmatrix} \begin{bmatrix} \Omega_2 - \frac{1}{LC} & -(\Omega_2 + \frac{1}{CR} + 1) \\ -(\Omega_1 - \frac{1}{LC}) & \Omega_1 + \frac{1}{CR} + 1 \end{bmatrix}$$

$$= \frac{1}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \times \begin{bmatrix} \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_1 t) - & \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) [\exp(\Omega_2 t) - \exp(\Omega_1 t)] \\ \left( \Omega_1 - \frac{1}{LC} \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) \exp(\Omega_2 t) & \\ \left( \Omega_2 - \frac{1}{LC} \right) \left( \Omega_1 - \frac{1}{LC} \right) [\exp(\Omega_1 t) - \exp(\Omega_2 t)] & - \left( \Omega_2 + \frac{1}{CR} + 1 \right) \left( \Omega_1 - \frac{1}{LC} \right) \exp(\Omega_1 t) + \\ & \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_2 t) \end{bmatrix}$$

The application of initial conditions:  $V_1(0) = V(0) = 0$  and  $V_2(0) = \mathcal{D}_t[V(0)] = \frac{1}{C}$  gives

$$\begin{bmatrix} V_1(t) \\ V_2(t) \end{bmatrix} = \frac{1}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \times \begin{bmatrix} \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_1 t) - & \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) [\exp(\Omega_2 t) - \exp(\Omega_1 t)] \\ \left( \Omega_1 - \frac{1}{LC} \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) \exp(\Omega_2 t) & \\ \left( \Omega_2 - \frac{1}{LC} \right) \left( \Omega_1 - \frac{1}{LC} \right) [\exp(\Omega_1 t) - \exp(\Omega_2 t)] & - \left( \Omega_2 + \frac{1}{CR} + 1 \right) \left( \Omega_1 - \frac{1}{LC} \right) \exp(\Omega_1 t) + \\ & \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_2 t) \end{bmatrix} \begin{bmatrix} 0 \\ \frac{1}{C} \end{bmatrix}$$

Or

$$\begin{bmatrix} V_1(t) \\ V_2(t) \end{bmatrix} = \frac{1}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \begin{bmatrix} \frac{1}{C} \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) [\exp(\Omega_2 t) - \exp(\Omega_1 t)] \\ \frac{1}{C} \left[ - \left( \Omega_2 + \frac{1}{CR} + 1 \right) \left( \Omega_1 - \frac{1}{LC} \right) \exp(\Omega_1 t) + \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_2 t) \right] \end{bmatrix}$$

This results

$$V_1(t) = \frac{\frac{1}{C} \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) [\exp(\Omega_2 t) - \exp(\Omega_1 t)]}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)}$$

Or

$$V(t) = \frac{\frac{1}{C} \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) [\exp(\Omega_2 t) - \exp(\Omega_1 t)]}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)}$$

Or

$$V(t) = \frac{\frac{1}{C} \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 + \frac{1}{CR} + 1 \right) [\exp(\Omega_1 t) - \exp(\Omega_2 t)]}{(\Omega_1 - \Omega_2) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \dots \dots \dots (14)$$

And

$$V_2(t) = \frac{\frac{1}{C} \left[ - \left( \Omega_2 + \frac{1}{CR} + 1 \right) \left( \Omega_1 - \frac{1}{LC} \right) \exp(\Omega_1 t) + \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_2 t) \right]}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)}$$

Or

$$\mathcal{D}_t[V(t)] = \frac{\frac{1}{C} \left[ - \left( \Omega_2 + \frac{1}{CR} + 1 \right) \left( \Omega_1 - \frac{1}{LC} \right) \exp(\Omega_1 t) + \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_2 t) \right]}{(\Omega_2 - \Omega_1) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)}$$

Or

$$\mathcal{D}_t[V(t)] = \frac{\frac{1}{C} \left[ \left( \Omega_2 + \frac{1}{CR} + 1 \right) \left( \Omega_1 - \frac{1}{LC} \right) \exp(\Omega_1 t) - \left( \Omega_1 + \frac{1}{CR} + 1 \right) \left( \Omega_2 - \frac{1}{LC} \right) \exp(\Omega_2 t) \right]}{(\Omega_1 - \Omega_2) \left( \frac{1}{LC} + \frac{1}{CR} + 1 \right)} \dots \dots \dots (15)$$

Using equations (7) and (8), we can find

$$(\Omega_1 + \frac{1}{C\mathcal{R}} + 1) (\Omega_2 + \frac{1}{C\mathcal{R}} + 1) = \left( -\frac{1}{2C\mathcal{R}} + \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} + \frac{1}{C\mathcal{R}} + 1 \right) \left( -\frac{1}{2C\mathcal{R}} - \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} + \frac{1}{C\mathcal{R}} + 1 \right)$$

Or

$$(\Omega_1 + \frac{1}{C\mathcal{R}} + 1) (\Omega_2 + \frac{1}{C\mathcal{R}} + 1) = \left( 1 + \frac{1}{C\mathcal{R}} + \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right) \left( 1 + \frac{1}{C\mathcal{R}} - \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right)$$

Or

$$(\Omega_1 + \frac{1}{C\mathcal{R}} + 1) (\Omega_2 + \frac{1}{C\mathcal{R}} + 1) = \left( 1 + \frac{1}{C\mathcal{R}} \right)^2 - \left( \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right)^2$$

On simplification of the right-hand side of this equation, we obtain

$$(\Omega_1 + \frac{1}{C\mathcal{R}} + 1) (\Omega_2 + \frac{1}{C\mathcal{R}} + 1) = \left( \frac{1}{LC} + \frac{1}{C\mathcal{R}} + 1 \right) \dots \dots \dots (16)$$

And

$$(\Omega_1 - \Omega_2) = -\frac{1}{2C\mathcal{R}} + \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} - \left( -\frac{1}{2C\mathcal{R}} - \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right)$$

On simplification of the right-hand side of this equation, we obtain

$$(\Omega_1 - \Omega_2) = \frac{1}{C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \dots \dots \dots (17)$$

Using equations (16) and (17) in equation (14), we get

$$V(t) = \frac{\frac{1}{C} [\exp(\Omega_1 t) - \exp(\Omega_2 t)]}{\frac{1}{C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}}$$

Or  $V(t) = \frac{I[\exp(\Omega_1 t) - \exp(\Omega_2 t)]}{\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}} \dots \dots \dots (18)$

Substituting equations (7) and (8) in equation (18), we get

$$V(t) = \frac{I \left\{ \exp \left[ \left( -\frac{1}{2C\mathcal{R}} + \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right) t \right] - \exp \left[ \left( -\frac{1}{2C\mathcal{R}} - \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right) t \right] \right\}}{\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}}$$

Or

$$V(t) = \frac{I \exp(-\frac{1}{2C\mathcal{R}}t) \left\{ \exp \left[ \left( \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right) t \right] - \exp \left[ \left( -\frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} \right) t \right] \right\}}{\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}} \dots \dots \dots (19)$$

This equation (19) provides an expression for the voltage across a parallel  $L - C - \mathcal{R}$  network connected to an excitation source providing a constant current and confirms that the presence of an inductor and a capacitor in the parallel  $L - C - \mathcal{R}$  network leads to variation in the voltage across the network even if the excitation source connected to the network provides a constant current, and that voltage across the parallel  $L - C - \mathcal{R}$  network depends on the quantity  $\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}$ , whether it is real, zero or imaginary. The value of quantity  $\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}$ , in turn, depends on the values of  $\frac{1}{\mathcal{R}^2}$  and  $\frac{4C}{L}$ . We have the following three possibilities:

**Possibility I:** If the values of network elements  $L, C$  and  $\mathcal{R}$  are so chosen that  $\frac{1}{\mathcal{R}^2} > \left(\frac{4C}{L}\right)^{\frac{1}{2}}$ , then the quantity  $\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}$  is real. In such a case, equation (19) can be rewritten as

$$V(t) = \frac{2I \exp(-\frac{1}{2C\mathcal{R}}t) \sinh \left( \frac{1}{2C}\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}} t \right)}{\sqrt{\frac{1}{\mathcal{R}^2} - \frac{4C}{L}}} \dots \dots \dots (20)$$

It is confirmed from the equation (21) that the voltage across the parallel  $L - C - \mathcal{R}$  network is non-oscillatory since sinh is non-periodic function, and it decays gradually to zero.

**Possibility II:** If the values of network elements  $L, C$  and  $R$  are so chosen that  $\frac{1}{R} = \left(\frac{4C}{L}\right)^{\frac{1}{2}}$ , then the quantity  $\sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  is zero. In such a case, equation (19) reveals that the current in the series  $L - C - R$  network is indeterminate, which is impossible. If the quantity  $\sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  is so small that it approaches to zero, then on expanding the exponential terms containing the quantity  $\sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  and taking only the first two terms, we can rewrite equation (19) as

$$V(t) = \frac{I \exp\left(-\frac{1}{2CR}t\right) \left\{ 1 + \left(\frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}}\right)t - \left[ 1 - \left(\frac{1}{2C} \sqrt{\frac{1}{R^2} - \frac{4C}{L}}\right)t \right] \right\}}{\sqrt{\frac{1}{R^2} - \frac{4C}{L}}}$$

Or

$$V(t) = \frac{I}{C} t \exp\left(-\frac{1}{2CR}t\right) \dots\dots\dots (21)$$

It is confirmed from the equation (21) that the voltage across the parallel  $L - C - R$  network is non-oscillatory and it decays to zero in the minimum time.

**Possibility III:** If the values of network elements  $L, C$  and  $R$  are so chosen that  $\frac{1}{R} < \left(\frac{4C}{L}\right)^{\frac{1}{2}}$ , then the quantity  $\sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  is imaginary. We can write the quantity  $\sqrt{\frac{1}{R^2} - \frac{4C}{L}}$  as

$$\sqrt{\frac{1}{R^2} - \frac{4C}{L}} = i \sqrt{\frac{4C}{L} - \frac{1}{R^2}} \dots\dots\dots (22)$$

Using equation (22), we can rewrite equation (19) as

$$V(t) = \frac{I \exp\left(-\frac{1}{2CR}t\right) \left\{ \exp\left[\left(\frac{1}{2C} i \sqrt{\frac{4C}{L} - \frac{1}{R^2}}\right)t\right] - \exp\left[\left(-\frac{1}{2C} i \sqrt{\frac{4C}{L} - \frac{1}{R^2}}\right)t\right] \right\}}{\sqrt{\frac{1}{R^2} - \frac{4C}{L}}}$$

Or

$$V(t) = \frac{2I \exp\left(-\frac{1}{2CR}t\right) \sin\left[\left(\frac{1}{2C} \sqrt{\frac{4C}{L} - \frac{1}{R^2}}\right)t\right]}{\sqrt{\frac{4C}{L} - \frac{1}{R^2}}} \dots\dots\dots (23)$$

It is confirmed from the equation (23) that the voltage across the parallel  $L - C - R$  network is oscillatory and its amplitude  $\frac{2I \exp\left(-\frac{1}{2CR}t\right)}{\sqrt{\frac{4C}{L} - \frac{1}{R^2}}}$  is decreasing exponentially with time, and its oscillating frequency is  $\frac{1}{4\pi C} \sqrt{\frac{4C}{L} - \frac{1}{R^2}}$ .

#### IV. CONCLUSIONS

In this paper, we have obtained the response of a parallel  $L - C - R$  network connected to an excitation source providing a constant current by matrix method. The discussion concludes that the nature of response (i.e. voltage) can be oscillatory or non-oscillatory depending on the values of elements  $L, C$  and  $R$  of the network. The nature of voltage can be made oscillatory if values of network elements  $L, C$  and  $R$  are so chosen that  $\frac{1}{R} < \left(\frac{4C}{L}\right)^{\frac{1}{2}}$ , and in this situation, the amplitude decreases exponentially with time and the frequency of oscillation is independent of excitation source providing a constant current. The nature of voltage is non-oscillatory if values of network elements  $L, C$  and  $R$  are so chosen that  $\frac{1}{R} > \left(\frac{4C}{L}\right)^{\frac{1}{2}}$  or  $\frac{1}{R}$  is slightly greater than  $\left(\frac{4C}{L}\right)^{\frac{1}{2}}$  and in these situation, the amplitude decays gradually to zero.

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