

Tribological Behaviour Of Laser Surface Textured AISI 52100 Steel

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Abstract : AISI 52100 is a standard grade Alloy steel. Increase in the lifetime of a component is done either by alloying with numerous appropriate materials before its producing. This study makes an attempt to enhance the service lifetime of AISI 52100 steel by modifying the surface through laser surface texturing process. And then wear tests were performed during a pin on disc equipment as per ASTM G-99 standard. The coefficient of friction, the wear rate and wear coefficient were determined on uncoated and laser surface textured pins. Finally determine good wear properties material is uncoated or laser textured material.

Keywords — AISI 52100, Coefficient of friction, Laser surface texturing, Uncoated, Wear rate, Wear properties.

I. INTRODUCTION

The principal aim of laser surface texturing to reduce the wear rate, coefficient of friction of the material and increase the lifetime of material. R. Kumutha & S. Ilaiyavel [1] To increase the life time of the component to determine the wear rate, coefficient of friction to compare and better material chosen at uncoated and coated material using wear testing method. SP Joshua, PD Babu[2] To improve the durability American iron and steel institute 52100 chromium steel in this work the effect of laser surface texturing analyzed with the different patterns of circles and ellipse comparing with untextured samples the wear behavior was investigated using the pin on disc tribometer. P Sivaiah, U Bodicherla [3] In the experimental investigation three types of cutting were considered two ware surface textured tools and third nontexture tool. taguchi analysis was carried out the performance during machining of AISI 52100 steel under MQL cooling condition. To determine the low surface roughness and tool flank wear. P Sivaiah, M Guru Prasad, M Singh [4] In this work textured tools performance was evaluated during turning of AISI 52100 steel under MQL and compared the obtained results with the untextured tools under MQL conventional cooling techniques. Y Gerbig, G Dumitru, V Romano, V Spassov [5] The tribological performance of

laser textures was studied as function of the pore depth and diameter unidirectional sliding test and the laser textured surfaces tested under those condition were produced by a well established na laser technique using Q switched Nd:YAG laser.

II. EXPERIMENTAL PROCEDURES

A. Material Properties

Alloy steels contain different varieties of steels that exceed the composition limits of Mn, C, Mo, Si, Ni, Va, and B set for carbon steels. AISI 52100 alloy steel is known as a high carbon, chromium containing low alloy steel. The chemical, physical, mechanical compositions are given in tables.

Table.1 Chemical Composition

ELEMENT	CONTENT(%)
Iron, Fe	96.5 - 97.32
Chromium, Cr	1.30 - 1.60
Carbon, C	0.980 - 1.10
Manganese, Mn	0.250 - 0.450
Silicon, Si	0.150 - 0.300
Sulfur, S	≤ 0.0250
Phosphorous, P	≤ 0.0250

B. Laser Surface Texturing

The length of material is 25mm and diameter of the material is 8mm. And the material is before laser texturing process we have develop the circular square pattern in AUTO CAD Software for laser texturing purpose. First AUTO CAD software opened in laptop and new file is selected, 10mm dia circle drawing drawn. And small size of circle, square are draw at 10mm circle. The small circle diameter is 0.5mm and small square side length is 0.25mm. The small circle and square horizontal distance is 1.5mm and vertical distance is 1mm. And number of small circle, square are drawn in 10mm circle. The each small circle, square is 'hatch' comment is used to form lines. And the HATCH line distance is 0.020mm. The HATCH line are converted to individual line by using explend comment. And the process is saved at pattern 1.dxf file format.



Figure 1. Laser Surface Texturing Machine

C. Wear Test

Wear performance of materials are commonly obtained from testing carried out in pin-on-disc equipment to ASTM G99 standard procedure. The photographic view of the pin on the disc is shown in. It gives a laboratory standard method to carry out sliding and abrasion wear tests. The tests were carried out under 10 N applied load and for sliding velocity of 0.3 m/s for a constant sliding radius of 10 mm. In all the cases coefficient of friction, wear rate and wear coefficient value are noted in uncoated material and laser surface textured material.



Figure 2. Wear Testing Machine

III. RESULT AND DISCUSSIONS

A. Coefficient Of Friction

Test procedures were employed with the pin on disc tests at 0.3m/s. The wear, Frictional Force and time were obtained at a load of 10 N for every 10 min sliding. The Plot of friction coefficient versus sliding distance for the uncoated, laser texturing are shown in Figure 5.1. This shows the Characteristic feature of the diagrams is that the friction coefficient values decreases as the Sliding distance increases at laser surface texturing. The dry friction of uncoated material around 0.9 and laser surface texturing can decrease the friction coefficient by 0.807.

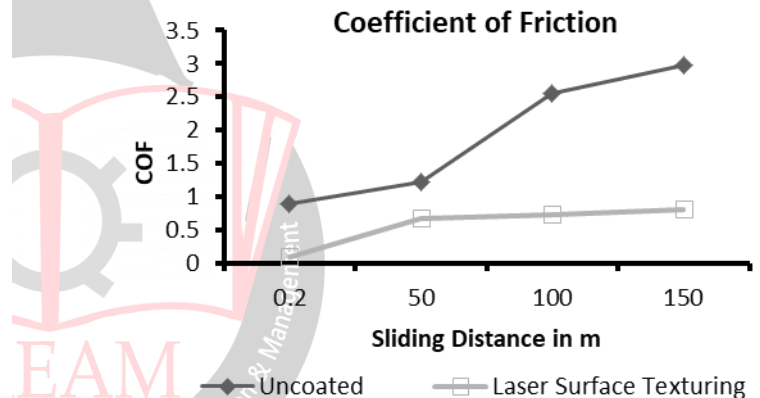


Figure 3. Coefficient of Friction

B. Wear Coefficient

Steady-state wear was proposed by Archard $V=K_sPL/3H$ where V is the volumetric loss of material after sliding for a distance L and load P normal to the wear surface. H is the Brinell hardness number of the pin while K_s a dimensionless standard wear coefficient. For known values of V, P, L, and H the standard wear coefficient can be calculated from the equation $K_s=3HV/PL$. Volumetric wear loss can be calculated from the weight loss W and the density. L. J. Yang expressed that the higher initial running – in wear rate, has a higher value initially in the transient wear regime and will reach a steady – state value when the wear rate becomes constant. Figure 5.2 shows the variation of wear coefficient with sliding distance. It is observed that wear coefficient decreased due to increase sliding distance. However under the same conditions laser surface texturing material is low wear coefficient.

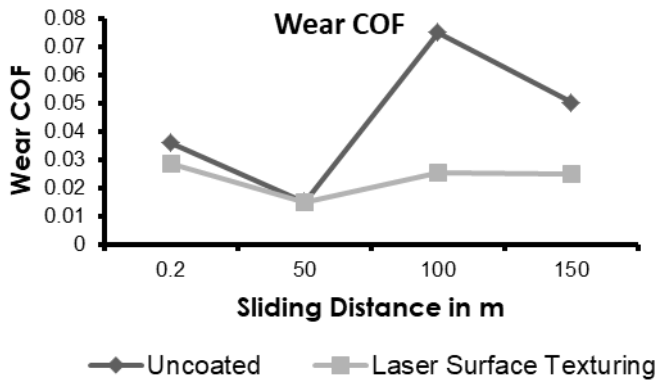


Figure 4. Wear COF

C. Wear Rate

The wear rate is calculated from the equation:

$$\text{Wear Rate} = \text{Volumetric Wear Loss} / \text{Sliding Distance.}$$

Wear rate of laser texturing compared uncoated material

Very less Wear loss. In pins and it exhibits the less Wear rate.

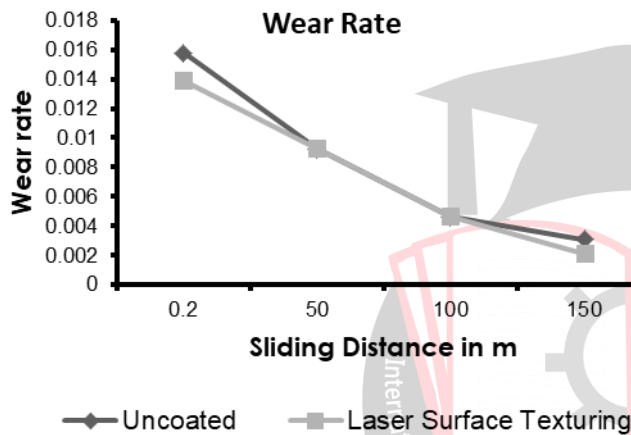


Figure 5. Wear Rate

IV. CONCLUSION

The Wear coefficient of uncoated, laser textured material were examined under 10 N loads at sliding velocity of 0.3m/s using a pin on disc apparatus and the results are summarized as follows:

- Laser surface textured material shows very low coefficient of friction compared uncoated material. The coefficient of friction is around 0.807 under 10 N loads with sliding velocity of 0.3 m/s. The reason is laser surface textured has improved its properties in terms of both frictions and wear.
- Laser surface textured material shows very low Wear coefficient compared with uncoated material. The Wear coefficient of friction is around 0.0250 under 10 N loads with sliding velocity of 0.3 m/s.
- Wear rate of laser surface textured material is lesser than uncoated material because of Very less Wear loss.

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